

1. TITLE OF THE INVENTION: A method to produce a glass fiber interior material

2. CLAIM

A method to produce a glass fiber interior material by pressurizing and heating a glass fiber mat to which uncured binder is added, the method comprising:

providing a set of metal molds which are arranged so as to form, in the internal(center) area of the interior material surface, at least one high density concave part having predetermined shape and a density of 200-500 kg/m<sup>3</sup> and at least one low density convex part surrounding the at least one high density concave part and having a density of 150-80 kg/m<sup>3</sup> and, in the peripheral area of the interior material surface, a high density concave part surrounding the at least one low density convex part and having a density of 200-500 kg/m<sup>3</sup>, wherein the entire circumference of the at least one low density convex part is substantially surrounded by the high density concave part, and wherein, for any arbitrary point in the at least one low density convex part, there is at least one point which belong to the high density concave part in each of four directions from the arbitrary point within the distance  $\ell$  which is obtained by the next formula

$$\ell = k \times D \ell (D h - D \ell)$$

herein,

$\ell$ : length or distance (mm)

Dh: Density of high density concave part (kg/m<sup>3</sup>)

D $\ell$ : Density of low density convex part (kg/m<sup>3</sup>)

k: a constant number (0.01 to 0.02);

pressurizing and heating by utilizing the metal molds.

3. DETAILED DESCRIPTION OF THE INVENTION

The present invention relates to the method for manufacturing the glass fiber interior material, particularly the interior material having concave-convex patterns in large size.

Mineral matter interior material having concave-convex patterns in large dimension of about 5 cm or more, for example, ceiling board, can give

gorgeous impression and at the same time, it has noncombustibility and is preferable as interior material. This type of interior material was conventionally manufactured by subjecting the original sheet having a certain density and thickness to a cutting process. However, the above cutting method is not only troublesome but it also decreases the strength of concave parts to be cut down; in addition, it easily develops a crack from the proximity of cutting boundary surface by the notch effect and it becomes necessary to back up the whole of the back of interior material to compensate the decreased strength, thus increasing the weight of interior materials per unit area, and when such interior material is used for the ceiling, there were drawbacks such as the need to obtain great strength of beams.

Attempts were made to save the trouble of cutting process by using the mold having predetermined concave-convex patterns to pressurize and heat the glass fiber mat so that the density of each parts are inversely proportional to the thickness and so that the decrease of the strength in concave parts due to the thinning of thickness is compensated by increasing the density of concave parts. In this method, wrinkles will be formed on the convex parts which maintain low density to provide sound absorbability and heat insulating property, and it becomes necessary to carry out smoothing process on the surface in order to use the material as the interior material.

Larger the size (area) of the convex parts, the greater the chance that wrinkles will occur. When many small concave-convex are in proximity with each other, they are not very apparent even if some of them occur, and it would not ruin the aestheticity. Therefore, this method (direct forming method) can produce interior material having small concave-convex but it would be extremely difficult to produce interior material having large concave-convex without wrinkles.

In order to solve such problems and to manufacture the interior material having concave-convex in large sizes without wrinkles by the direct forming method, the present inventors conducted considerable amount of studies. As a result, the present inventors propose the present invention which has been ascertained to be advantageous.

The present invention is a method to produce a glass fiber interior material by pressurizing and heating a glass fiber mat to which uncured binder is added, the method comprising:

providing a set of metal molds which are arranged so as to form, in

the internal area of the interior material surface, at least one high density concave part having predetermined shape and a density of 200-500 kg/m<sup>3</sup> and at least one low density convex part surrounding the at least one high density concave part and having a density of 150-80 kg/m<sup>3</sup> and, in the peripheral area of the interior material surface, a high density concave part surrounding the at least one low density convex part and having a density of 200-500 kg/m<sup>3</sup>, wherein the entire circumference of the at least one low density convex part is substantially surrounded by the high density concave part, and wherein, for any arbitrary point in the at least one low density convex part, there is at least one point which belong to the high density concave part in each of four directions from the arbitrary point within the distance  $\ell$  which is obtained by the next formula

$$\ell = k \times D \ell (D h \cdot D \ell)$$

herein,

$\ell$ : length or distance (mm)

Dh: Density of high density concave part (kg/m<sup>3</sup>)

D $\ell$ : Density of low density convex part (kg/m<sup>3</sup>)

k: a constant number (0.01 to 0.02);

pressurizing and heating by utilizing the metal molds.

Next, the present invention will further be explained in detail.

In the present invention, the uncured glass fiber mat, which is produced by spraying glass short fibers manufactured by centrifugation, fire flame method, etc. with binder and then accumulating the glass short fibers on the perforated conveyer, is used as the glass fiber mat. The type of binders is not limited; for example, binders of phenolic resin type, urea resin type, and melamine resin type can be used. The appropriate amount to be used is about 7-15 wt % to the glass fibers as a solid content. The thickness of the mat (weight per unit area) is determined according to the thickness and density of the desired interior material but those having a thickness of about 0.3-2 kg/m<sup>2</sup> are normally used.

Mat is put on a lower mold 3 having concave-convex, which corresponds to concave-convex on the interior material surface, on a predetermined position. The mat is then pressed with an upper mold 4, and during the press the heating is conducted.

In this instance, the distance between the lower mold 3 having concave-convex and flat upper mold 4 is determined so that the density of

high density concave parts 1 is between 200-500 kg/m<sup>3</sup>. By setting the density of concave parts within this range, a sufficient strength is provided to the concave parts, and furthermore, no wrinkles will be formed on the concave parts. The glass fibers are compressed with strong force and as a result, the formed wrinkles are crushed and smoothed out.

The distance between the upper mold and lower mold is determined so that the density of low density convex part 2 is between 150-80 kg/m<sup>3</sup>. The density is set within the above range so as to provide sound absorbability, heat insulating property and strength necessary for the interior material.

When the densities are set within the above range, however, the wrinkles will easily occur on the low density convex part if the concave-convex pattern is large and the resulting interior material cannot be used as it is; it would be necessary to polish the surface. Even when painting the surface or adhering a material for the surface, a beautiful surface cannot be obtained if the surface with wrinkles are used as it is.

As a result of studies to solve the concerned problems, the present inventors found that the occurrence of wrinkles can be prevented by determining the shape of the mold so that the low density convex part 2 is surrounded by the high density concave part 1, and that, for any arbitrary point P in the low density convex part, there is at least one point (Q, R, S and T in figure 2) which belong to the high density concave parts in each of four directions from the arbitrary point P within the distance  $\ell$  ( $\ell_1$ - $\ell_4$  in figure 2)(mm) which is  $k \times D \ell$  ( $D$  h ·  $D \ell$ ); and pressurizing and heating the glass fiber mat by utilizing the mold so as to cure the glass fiber mat.

In the formula,  $D_h$  and  $D_l$  are densities of high density concave parts and low density convex part represented in kg/m<sup>3</sup>.  $k$  is a constant number which is determined within the range of 0.01-0.02 according to a type of mat, desired smoothness, etc. The smaller the  $k$ , the larger the smoothness (thus, the occurrence of wrinkles are small), and especially preferable result can be obtained by  $k = 0.01$ .

Although the mechanism of the present invention is not sufficiently clear, as a result of the high pressurization of the high density parts, the mat surface of low density part are stretched as in the arrow X and Y in Fig. 2 toward the high density parts by the mold parts that press the high density parts. In this state where the tensile forces are applied, the pressurization and heating are conducted. The tensile forces become greater toward the

proximity of the high density parts. As the low density part is surrounded by the high density parts, all point P belonging to the low density part are pressurized in a tense state where they are pulled from four directions. As this tensile forces become greater as it distances itself from the center part of the low density part (as it nears the high density parts), it is considered that pressurization and heating are carried out without occurrence of sagging on the mat surface, and thereby the occurrence of wrinkles is prevented as well. The tensile force acting on the low density part tend to become less as the distance between the low density part and the high density parts becomes longer. The tensile force acting on the low density part tend to become greater as the difference in height of the surface, which relates to the difference in the density, between the low density part and the high density parts becomes greater. Furthermore, wrinkles tend to easily occur as the density of the low density part becomes lower. As a result of the experiment, it was found that the wrinkle occurrence can be prevented by setting  $\ell$  equal to or less than  $k \times D \ell (D h - D \ell)$ . If  $\ell$  is too large, the wrinkle occurrence cannot be sufficiently prevented.

According to the method of the present invention, a light-weight interior material having concave-convex of about 50 cm or more with no wrinkles can easily be manufactured without finishing the surface by polishing. Thus, the present invention is industrially useful. However, the present invention is not limited to the above explanations and following example; it can be changed as appropriate within a range that do not depart from the purpose and the spirit of the present invention. For example, the interior material manufactured by the method of the present invention can be subjected to the finishing such as surface painting and other processing. Or, the interior material manufactured by the method of the present invention can be cut as appropriate so that the ends become the low density part. Furthermore, a plurality of independent low density part and high density parts can be formed as well.

The density of the low density part and high density parts may not be constant but different depending on places. A plural of internal high density parts may be formed. In the internal area, high density parts may be formed as shown in figure 3, not at the center as shown in figure 1.

An example of the present invention is shown below.

A glass fiber mat with 10 wt % binder contents (as a solid content),

1.2 kg/m<sup>3</sup>, thickness of 12 mm is obtained by spraying phenolic binder on the glass short fibers manufactured by centrifugation and then accumulating them on the perforated conveyor. The glass fiber mat is pressurized by molds 3 and 4 as shown in Fig. 2 and heated for one minute at 250 °C to be cured. As a result, a ceiling board without wrinkles is obtained.

The dimensions of the ceiling board at this example are as follows:

High density concave part in the internal area

Size 75 mm x 100 mm

Thickness 3 mm

Density 400 kg/m<sup>3</sup>

Low density convex part

The size of the outer circumference 225 mm x 300 mm

Thickness 12 mm

Density 100 kg/m<sup>3</sup>

High density part in the peripheral area

Width 10 mm

Thickness 3 mm

Density 400 kg/m<sup>3</sup>

The maximum value of  $\ell_1$ ,  $\ell_2$ ,  $\ell_3$  and  $\ell_4$  in the present example is 300 or less,  
 $0.01 \times 100 \times (400 - 100) = 300$ .

#### 4. BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 shows one example of the glass fiber interior material manufactured by the method of the present invention, Fig. 2 is a cross-sectional view of A-A direction showing the method for manufacturing the interior material of Fig. 1, Fig. 3 is a plain view similar to Fig. 1 but showing other examples of the present invention.

1 represents high density parts, 2 represents low density part, 3, 4 represents mold, 5 represents uncured glass fiber mat.

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硝子繊維内装材の製造法

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明 細 書

1. 発明の名称 硝子繊維内装材の製造法

D<sub>h</sub> : 高密度部D<sub>h</sub>の密度 (kg/cm<sup>3</sup>)

D<sub>l</sub> : 低密度部D<sub>l</sub>の密度 (kg/cm<sup>3</sup>)

2. 特許請求の範囲

n : 常数 (0.01 ~ 0.02)

未硬化の結合剤を含有した硝子繊維マツトを  
加圧、加熱して内装材を製造するに際し、内装  
材表面の内域に所定形状の密度200~500  
kg/cm<sup>3</sup>の高密度部と内域低密度部を交互密  
度150~80 kg/cm<sup>3</sup>の低密度部を形成せしめる  
とともに、この低密度部を囲んで密度200~  
500 kg/cm<sup>3</sup>の高密度部を形成せしめるよ  
う、且つ低密度部は高密度部で実質的にそ  
の金属を包繞され、又低密度部の任意の点に  
対し次式で求められる距離s以内で径径4方向  
に少くとも各一つの高密度部に属する点が存  
在するよう金属を配設し、この金属を使用して  
加圧、加熱を行なうことを特徴とする硝子繊維  
内装材の製造方法

$$s = x \times D \times s \{ D_h - D_l \}$$

但し

$$s : 距離 (mm)$$

3. 発明の詳細な説明

本発明は硝子繊維内装材、特に大きな寸法の  
凹凸模様を有する内装材の製造方法に関するも  
のである。

5mm程度乃至それ以上の大きなダイメンショ  
ンの凹凸模様を有する、裝飾質内装材例えば天  
井装は豪華な感じを与えることができ、且つ不  
燃性を有し内装材として好適なものである。こ  
の種内装材(凹凸内装材という)は従来一定密  
度、一定厚みの厚板を切削加工することによつ  
て製造されたが、上記方法(切削法と云う)は  
手数を要するばかりでなく切削される部部の密  
度が低下し、又切削境界面附近からノッチ効果  
によつて亀裂が発生しやすくなり、更に又密度  
低下を補うため内装材表面全体に磨耗をする  
必要が生じ、このため内装材単位面積当りの重  
量が増加し、この内装材を天井に吊した場合は

強度を大きくならしめることを要する等の欠点があった。

銅子繊維マツトを所定の凹凸模様を有する金型を使用して加圧、加熱して、各部分の密度を厚みに適比例せしめることにより、切削加工の平間を省き、且つ厚みを小さくしたことによる凹部の強度低下を凹部の密度を大きくすることにより補うことも試みられたが、この方法によるときは、所望の吸音性、断熱性を与えるため密度を高く保つた凸部に割が発生し、内装材として使用するためには表面を平滑加工する必要が生ずる。

割の発生は凸部の大きさ（面積）が大きい程大きくなる傾向があり、又小さい凹部が多級近接して配設されている場合は割が若干発生しても容易に立たず、強度を損うこともないので、この方法（直接成型法という）では、小さい凹部を有する内装材を製造することはできても、割のない大きい凹部を有する内装材を製造することは極めて困難である。

D<sub>1</sub> : 高密度凹部の密度 (Kg/cm<sup>3</sup>)

D<sub>2</sub> : 低密度凸部の密度 (Kg/cm<sup>3</sup>)

X : 常数 (0.01 ~ 0.02)

ことにより極めて好適な結果の得られることを見出し本発明として提案したものである。

次に本発明を更に具体的に説明する。

本発明において銅子繊維マツトとしては、溶心法、火増注等によつて製造された銅子繊維綿にバインダを塗布し、有孔コンベヤ上に集積した未硬化銅子繊維マツトを使用する。バインダの種類は特に限定はなく例えばフェノール樹脂系、炭素樹脂系、メラミン樹脂系バインダが使用できる。その使用量は凹形分として銅子繊維に対し7 ~ 15重量%程度とするのが適当である。マツトの厚み（単位面積当りの重量）は所望の内装材の厚み、密度に応じて定められるが、通常0.3 ~ 2.0g/cm<sup>2</sup>程度のものが用いられる。

マツトは所定位置に内装材表面凹凸に対応する凹部を有する下方金型3上に載置し、上方金型4で加圧、この間に加熱を行う。

本発明者はかかる短点を解決し、直接成型法によつて、割のない、大きい寸法の凹部を有する内装材を製造する為検討を重ねた結果未硬化の組合形を附与した銅子繊維マツトを加圧、加熱して内装材を製造するに際し、内装材表面の凹部に所定形状の密度200 ~ 500 Kg/cm<sup>3</sup>の内装材高密度凹部と内装材低密度部を両面密度150 ~ 300 Kg/cm<sup>3</sup>の低密度部を形成せしめるとともに、この低密度部を無んで密度200 ~ 500 Kg/cm<sup>3</sup>の周縁高密度凹部を形成せしめると、且つ低密度凸部は高密度凹部で実質的にその全周を覆われ、又低密度凸部の任意の点に対し次式で求められる距離X以内には4方向に少くとも各一つの高密度凹部に属する点が存在するよう金型を配設し、この金型を使用して加圧、加熱を行なうことを特徴とする銅子繊維内装材の製造方法。

$$X = x \times D \{ (D_1 - D_2) \}$$

但し

$$X : \text{距離} (\%)$$

この高密度凹部1は密度が200 ~ 500 Kg/cm<sup>3</sup>とするよう凹凸を有する下方金型3、平滑な上方金型4間の距離を定める。凹部の密度をこの範囲に定めることにより、凹部に充分な強度を与え、しかも凹部に割が発生することはない。銅子繊維が強く圧縮される結果、割が生じた後には割は、平滑化されるものと思われる。

低密度凸部2は密度が150 ~ 300 Kg/cm<sup>3</sup>となるよう上方、下方金型間の距離を定める。内装材に必要な吸音、断熱性及び強度を与えるために密度を上述の範囲とする。

しかしながら密度を上述の範囲とすると凹凸形状が大きい場合低密度凸部に割が生じ易く、内装材としてそのまま使用することではできず、表面を研磨する必要がある。表面に研磨し、或は表装材を貼着する場合でも割のある面をそのまま使用すると実質的な表面をうることはできない。

本発明者はかかる短点を解決する為検討を重ねた結果、低密度凸部2を高密度凹部1で周縁



し且つ低密度部内の任意の点Pに対しPとの距離(第2図では $A_1 \sim A_6$ )が $K \times D_2$  ( $D_2 = D_h - D_s$ )より小さい高密度部内にある点(第2図では $a, b, c$ 及び $T$ )がPのほかに四方に少くとも一つ存在するよう金型の形状を定め、この金型を用いて銅箔被覆マツトを加圧しつつ加熱し、硬化せしめることにより皺の発生を防止しうることを見出した。

お式式中 $D_1, D_2$ は $R_2$ が波わした当該高密度部及低密度部間の密度、 $K$ は電解でマツトの被覆所要の平滑度等に応じて $0.01 \sim 0.02$ の範囲で定められる係数である。 $K$ を小とするほど平滑度は大(従つて皺の発生は小)となり $K=0.01$ とすることにより特に良好な結果をうる事ができる。

本発明の作用については充分明らかではないが、高密度部が強く圧縮される結果、高密度部に対応する金型により低密度部に対応するマツト表面が高密度部に向つて第2図矢印 $S, T$ のようにより引張られ張力を受けし状態で加圧、加熱さ

れる。しかもこの引張り力は高密度部に近い部分程大きく又低密度部は高密度部で阻まれてゐるので、低密度部に属する点Pはすべて四方から引張られて緊張した状態で加圧され、しかもこの引張り力は低密度部の中心部から離れる程(高密度部に近い部)大となるので、マツト表面にたるみが生ずることなく加圧、加熱され皺の発生が防止されるものと思われる。尚、この低密度部の受ける引張り力は該低密度部と高密度部との距離が大となる程小となり又低密度部と高密度部の密度の差に对应する該低密度部の高さの差が大きくなる程大となる傾向があり更に又低密度部の密度が小さい程皺が発生しやすくなる傾向があり、実験の結果 $K \leq K_2$  ( $D_h - D_s$ )とすることにより皺の発生が防止しうる事が見出された。 $K$ があまり大きいと皺の発生を充分防止することはできない。

本発明の方法によるときは $500^\circ\text{C}$ 程度以上の凹凸を有する皺のない超量の内装材を所期による断面仕上げを施すことなく容易に製造する

ことができ、本発明は工業上有益なものであるが、本発明は上述の説明及び以下の実施例に限定されることなく、本発明の目的及精神を逸脱しない範囲において適宜変更できるものである。例えば本発明の方法によつて製造した内装材に表面塗層等の仕上げ、加工を施して使用してもよく、又、本発明の方法によつて製造された内装材を適宜切削し、所部が低密度部となるようににしてもよい。更に又、独立した低密度部、高密度部を多数設けることもできる。

尚、又例えば低密度部、高密度部の密度を一定とせず、連続的によつて密度を異ならしめてもよく、或は内装高密度部を複数個設け又は第2図に示すように内装高密度部を幾何學的中心的に設けることなく第2図に示すように配列してもよい。

次に本発明の実施例を示す。

銅箔材によつて製造された銅箔被覆マツトフェノール系バインダを噴射しつつ穿孔コンペマー上に集積して得られたバインダー含有量(面積

分として)10重量%、 $1.2 \text{ kg/m}^2$ 、厚み1.2%の銅箔被覆マツトを第2図に示すように並置し、4で加圧しつつ $250^\circ\text{C}$ にて1分間加熱して硬化せしめ皺のない天井板をうることができた。この際の天井板のディメンションは次の通りである。

#### 内装高密度部

大きさ	$75\% \times 100\%$
厚み	5%
密度	$400 \text{ kg/m}^2$

#### 低密度部

外周の大きさ	$72.5\% \times 98.8\%$
厚み	1.2%
密度	$100 \text{ kg/m}^2$

#### 連続高密度部

巾	10%
厚み	5%
密度	$400 \text{ kg/m}^2$

なお、本実施例にかかる $A_1$ の最大値は

$$350 \text{ 以下}, 0.01 \times 100 \times (4.88 - 100) = 3.00$$

